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PROPAGATION AND ATTENUATION OF Lg WAVES IN SOUTH AMERICA

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Observatorio San Calixto Cas. 5939 La Paz, Bolivia

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This technical report has been reviewed and is approved for publication.

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18 (cont'd) recording type, oceanic path, cordilleran path, transmission efficiency.

previous

10-(cont'd)

part Pwere revised. They confirm conclusions of part I and help to identify efficiency of different paths and type of Lg recording, since origin regions and recording stations are at the ends of wave path (figs. 12-14). Type of recording may unveil hidden cordileran structure in Andes-plains transition. ()

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Grant AFOSR-87-Ø311A PROPAGATION AND ATTENUATION OF Lg WAVES IN SOUTH AMERICA

SCIENTIFIC REPORT

INTRODUCTION

The seismic phase Lg had not been remarked by seismologists before Press and Ewing (1952) studies, in spite of its relevance in many short period records; possibly it was a part of a relative abandon of surface waves (which had been considered the main part of seismograms, but later they were of much less use than shorter smaller body waves).

Pomeroy et al. (1982) review the investigations achieved concerning Lg (together with other regional phases) considered potential discriminators between earthquakes and explosions; they list a generous bibliography, that we shall spare now.

A fact we have to emphasize: Lg has been studied mostly for ancient crustal paths, so that results generally are characterized by two qualities: relevance and uniformity, making them a good candidate for the measurements of seismic magnitude, especially for small events.

In South America a few Lg studies have been performed; we mention only Cabré (1971) and Chinn et al. (1980). The theses of Alcócer (1989) and Ayala (1989) and a paper of Minaya et al. (1989) are a fruit of this Grant and are synthesized in that report.

PART I. Lg AS RECORDED IN LPB STATION

Data used

486 earthquakes ocurred in or near South America and have been examined in La Paz, Bolivia, LPB station records, after rejecting those with oceanic path enough long to eliminate Lg and those deeper than 200 km. We consider earthquakes between 1974 and 1986, of magnitude mb between 4.4 and 5.8. (Epicenter determinations by the International Seismological Centre were used). Let us remark the uneven distribution of epicenters in the region, especially we have to emphasize the small number of earthquakes from the Brazil. See hypocentral data in Table I, together with azimuth to LPB and epicentral distance in degrees, hypocentral distance in km, velocity, normalized amplitude Lg/P (introduced later), time of Lg travel and character.

Table I

No.	-	DATE			Н		LAT	LON6	W H	ab	D	Az	٧	Lg/P	D	ī	CHAR
:	y	g	d	h	8	5	(0)	(o)	(ks)	(0)	(o)	ka/s)	(km)	(5)	

COLOMBIA

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1-75
      V 12 00 00 39.0 6.88N 73.09 59 4.6 23.78 168 3.65 2.7 2646.9 726.0 B
 2-75 VI 23 05 22 48.3 6.83N 73.11 162 4.9 23.73 168 3.65 5.6 2641.6 723.7 B
 3-76 II 21 23 23 36.3 8.48N 77.21 42 4.6 19.80 152 3.57 7.7 2119.3 593.7 A
 4-76 III 13 21 44 41.8 6.83N 72.98 166 5.3 23.71 168 3.69 1.8 2639.6 714.2 A
       V 12 16 42 15.1 7.43N 74.95 61 5.1 24.75 164 3.59 6.6 275D.6 810.9 A
 5-76
 6-76 VI 14 01 37 00.1 6.75N 73.0 161 4.8 23.64 168 3.55 1.9 2631.6 741.9 B
 7-76 VIII 03 02 19 22.7 5.23N 75.97 123 4.7 22.80 168 3.67 5.1 2533.1 689.0 B
      V 15 21 52 43.8 6.20N 77.44 6 4.7 24.41 168 3.54 1.1 2712.2 766.2 B
8-77
9-78
       I 10 20 08 36.1 3.51N 73.64 42 4.8 20.65 165 3.56 1.6 2294.8 644.9 C
12-78 IV 28 04 28 29.0 12.00N 72.54 13 5.2 28.68 170 3.57 1.8 3185.4 891.8 A
        V 27 16 16 42.5 6.76N 72.98 125 4.7 23.64 168 3.56 1.2 2631.9 739.4 B
12-78 VI 18 82 20 25.3 6.83N 72.9 169 4.1 23.70 168 3.62 2.3 2639.6 727.8 C
13-78 VIII 08 02 58 36.2 7.02N 72.11 39 5.0 23.73 170 3.55 8.3 2636.9 738.8 A
        X 85 23 22 21.0 7.36N 76.94 35 4.7 25.30 160 3.56 0.9 2811.3 789.7 C
14-78
15-79
       V 29 12 59 02.5 5.28N 75.73 122 4.9 22.95 161 3.64 1.8 2552.9 700.5 B
16-73 IX 02 02 00 12.4 4.28N 76.39 101 4.7 28.86 159 3.68 0.6 3474.2 944.0 C
17-80 II 12 08 18 49.4 3.65N 74.02 39 4.4 20.89 164 3.53 2.0 2329.4 657.6 B
18-80 III 06 13 42 03.0 5.97N 74.25 60 4.5 23.16 165 3.54 1.8 2574.8 728.0 B
19-80
       V 25 15 43 30.4 5,45N 74.50 33 5.0 22.47 164 3.56 3.1 2456.8 701.3 B
      XI 18 16 34 38.5 6.82N 72.92 17! 4.9 23.68 168 3.53 1.0 2636.6 746.5 B
29-86
21-80 XI 26 17 35 41.2 7.87N 72.40 46 4.9 24.62 170-3.55 9.1 2735.7 759.8 A
22-80 XI 27 06 50 50.0 10,90N 68.02 33 --- 27.29 180 3.59 5.5 3032.4 842.2 A
       IV 27 18 50 38.7 7.01N 75.52 33 4.9 24.87 160 3.58 1.4 2763.5 771.3 3
23-81
24-31
        V 13 04 38 25.0 4.10N 77.11 47 4.6 22.35 157 3.54 2.7 2483.7 701.6 C
25-81
        V 20 03 01 49.0 7.74N 76.31 136 4.5 22.64 159 3.59 1.0 2519.2 701.7 C
26-81 VI 13 18 39 23.9 6.78% 73.05 171 5.0 23.67 168 3.68 1.4 2635.5 715.1 8
27-81 VIII 05 12 58 28.0 3.98N 76.39 52 5.1 21.92 158 3.56 1.9 2435.3 685.0 A
28-81 VIII 25 16 54 35.0 6.95N 76.60 8 5.3 24.80 160 3.55 6.1 2755.5 775.0 C
29-81 VIII 30 20 50 9.4 6.91N 76.53 35 4.9 24.74 160 3.51 2.5 2749.1 783.6 C
18-98
       X 24 04 36 50.9 6.82N 73.00 167 4.9 23.71 168 3.51 1.3 2639.7 752.1 C
        X 26 09 05 29.8 5.79N 73.05 165 4.9 23.69 168 3.69 2.8 2637.4 714.2 C
32-81 XII 17 12 54 63.4 6.79N 73.65 165 5.0 23.68 168 3.67 0.8 2636.2 718.3 3
33-82 II 23 28 07 30.9 6.73N 73.01 175 4.7 23.62 168 3.56 2.6 2638.2 719.2 A
34-82 III 03 12 21 52.2 6.76N 72.96 178 4.7 23.63 168 3.58 1.8 2631.3 752.8 B
35-82 V 14 01 18 50.8 2.36N 75.50 63 4.6 20.13 159 3.52 2.6 2236.6 632.2 8
36-82 VII 12 13 35 42.8 4.34N 73.53 16 4.6 21.42 166 3.55 2.2 2380.8 670.8 C
37-82 VIII 15 87 26 28.3 6.74N 73.81 172 4.9 23.50 168 3.54 3.3 2616.7 739.7 C
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38-82 XII 23 22 47 2.4 6.87N 72.82 168 4.8 23.72 169 3.54 1.3 2648.1 723.6 C 39-83 I 10 17 02 27.5 6.76N 72.98 171 4.9 23.65 168 3.57 2.0 2645.2 737.5 A 40-83 III 07 23 14 11.4 6.86N 73.04 163 4.8 23.76 168 3.52 1.6 2644.8 751.6 C 41-83 III 31 13 12 51.0 2.50N 76.70 12 5.4 20.68 156 3.57 5.6 2297.8 634.0 A 42-83 VII 23 21 29 44.6 6.88N 73.06 160 4.5 23.78 168 3.54 2.3 2647.0 746.4 C 43-83 VII 24 15 39 45.6 6.82N 73.05 165 4.8 23.71 168 3.54 2.7 2639.6 746.4 C 44-83 VIII 29 08 24 24.7 6.80N 73.0 169 5.0 23.70 168 3.55 4.4 2638.5 721.3 A 45-83 XII 31 12 18 5.5 6.82N 73.02 170 4.7 23.70 168 3.54 0.8 2636.8 744.5 C 46-84 I 06 11 37 49.8 6.75N 73.06 166 5.0 23.66 168 3.59 4.7 2630.8 733.2 C 47-84 I 25 18 46 25.0 3.50N 76.66 49 4.6 21.62 157 3.53 3.4 2402.7 600.0 C 48-84 I 28 17 04 39.2 6.66N 74.52 81 5.0 23.91 165 3.50 1.7 2657.9 758.5 8 49-84 VIII 11 13 14 20.9 6.76N 72.99 173 4.7 23.65 168 3.65 1.3 2633.4 721.1 B 50-84 X 27 11 56 13.2 9.32N 74.73 61 5.0 26.99 166 3.68 0.5 2999.5 815.1 C

VENEZUELA

1-74 I 25 21 51 48.0 11.00N 61.00 27 4.4 27.93 194 3.52 3183.4 882.8 A 2-74 VI 12 16 25 45.2 10.60N 63.47 11 5.7 27.35 198 3.66 1.8 3038.9 829.8 A VI 13 12 32 31.0 10.61N 63.35 8 --- 27.37 193 3.57 8.4 3040.8 852.0 B IX 28 14 47 57.9 9.35N 70.57 41 4.7 25.83 175 3.54 3.6 2878.3 812.1 8 X 29 93 19 16.9 10.58N 63.45 33 5.9 27.33 191 3.62 1.1 3036.8 839.1 A 6-75 III 85 13 47 58.3 9.13N 69.87 25 5.5 25.56 176 3.65 5.6 2848.1 779.7 C 7-75 III 05 15 18 14.8 9.17N 69.91 43 4.5 25.60 176 3.51 4.3 2844.7 810.2 B 8-75 IV 05 09 34 37.6 10.10N 69.95 36 5.5 26.43 177 3.66 2.7 2936.8 802.4 B IV 15 09 47 44.8 9.42N 61.47 52 5.3 26.61 194 3.63 3.4 2957.1 814.6 B 18-75 VII 18 05 17 33.0 10.94N 64.46 3 4.8 27.53 188 3.66 6.1 3858.8 836.0 B 11-75 VIII 24 01 05 15.1 10.75N 62.65 111 5.1 27.54 191 3.59 2.0 3073.1 854.9 A 12-75 XII 05 09 31 50.8 10.83N 62.67 144 4.9 27.71 191 3.63 4.6 3062.2 849.2 A X 13 17 35 50.7 10.81N 61.53 63 4.9 27.93 194 3.65 1.6 3103.9 815.3 A XII 02 05 33 59.3 10.78N 63.71 38 4.8 27.19 177 3.63 2.9 3021.3 832.7 B 15-76 XII 21 04 32 31.0 8.80N 61.70 48 4.7 25.92 194 3.68 1.9 2888.0 783.0 A I 26 05 43 22.8 7.50N 71.95 75 4.6 24.18 171 3.51 1.2 2687.7 766.2 B II 21 03 07 43.5 10.52N 62.51 45 4.7 27.45 192 3.58 1.5 3050.3 850.5 B II 21 17 48 1.0 9.55N 76.81 4 5.0 26.00 174 3.53 4.6 2888.8 819.0 B 19-77 VII 24 05 44 44.3 10.82N 68.79 14 4.6 27.19 179 3.53 9.0 3021.1 855.7 A 28-77 VIII 14 04 22 49.7 18.94N 62.36 118 4.2 27.87 192 3.65 5.9 3098.6 831.3 B IX 83 15 25 16.1 18.42N 62.28 35 4.7 27.39 192 3.54 7.6 3843.5 857.9 B 1X 14 20 51 8.8 10.85N 62.38 34 4.7 27.79 192 3.51 1.3 3098.2 882.7 B 23-77 IX 18 17 31 16.2 10.51N 63.33 42 4.6 27.28 190 3.55 7.2 3031.4 853.8 B X 64 13 44 54.7 18.38% 62.32 42 5.1 27.34 142 3.55 1.3 3838.8 855.8 C 25-77 XII 11 16 22 6.2 9.56N 69.52 2 5.5 25.70 177 3.56 6.4 2855.5 801.3 B 26-77 XII 17 23 25 18.8 18.99N 65.58 14 4.6 27.38 186 3.54 3.5 3042.2 859.4 A I 18 01 17 54.5 10.26N 62.19 46 4.8 27.26 192 3.59 2.2 3023.2 842.5 B 28-78 III 15 15 26 37.8 18.33N 62.25 11 4.5 27.31 192 3.62 2.5 3034.4 839.0 C 29-78 V 18 @3 25 4.9 10.76N 62.45 116 4.7 27.68 192 3.65 1.2 3077.7 '.1 B 38-78 XI 07 02 48 23.0 8.57N 62.90 17 4.6 25.46 192 3.55 1.9 2828.9 797.0 A 31-79 III 38 12 10 07.8 12.89N 78.79 33 4.6 29.36 175 3.53 1.2 3262.3 923.8 B 32-79 V 05 20 04 56.8 8.43N 70.91 08 5.4 24.96 174 3.53 8.6 2773.3 784.4 B V 05 20 08 40.3 8.48N 70.99 34 5.2 25.01 173 3.65 5.0 2777.9 760.7 A

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34-79 VII 17 08 49 28.8 10.25N 62.24 48 4.6 27.00 193 3.54 6.6 3000.2 847.2 A
35-79 VIII 03 11 43 57.3 8.73N 70.76 15 4.8 25.24 174 3.68 1.4 2837.8 720.7
      II 12 02 29 14.0 9.05N 68.62 24 4.6 26.21 173 3.54 1.9 2912.3 822.0 A
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49-88
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42-81 XII 08 22 53 13.3 3.03N 71.06 43 4.5 25.57 173 3.50 1.6 2841.4 811.8 B
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45-82 III 18 02 11 50.0 10.50N 62.40 58 4.5 27.44 192 3.57 1.6 3049.4 855.0 B
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59-86
       II 26 11 41 15.0 9.72N 61.37 62 4.5 26.92 194 3.56 2.8 2991,7 840.4 B
      II 28 01 12 56.8 9.64N 61.39 45 4.5 26.83 194 3.60 2.8 2981.4 828.2 8
68-86
61-86 III 25 67 18 33.6 10.35N 62.53 10 4.7 27.27 192 3.52 2.8 3030.8 860.8 8
62-86 VI 11 13 48 4.0 10.60N 62.93 33 4.9 27.44 191 3.58 10.3 3049.i 864.3 A
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ARGENTINA

1-74 I 97 16 35 5.6 26.878 65.78 28 5.7 18.54 347 3.61 1.9 1171.3 324.5 C 2-74 I 11 05 18 0.9 31.965 68.85 108 5.2 15.09 10 3.62 0.1 1680.1 464.1 C 3-74 1 23 21 43 49.4 32.235 69.82 103 5.2 15.70 5 3.50 1.2 1747.5 485.6 C 4-74 II 14 06 19 56.6 26.135 66.36 48 4.9 9.69 358 3.63 0.5 1877.4 296.5 B II 20 03 02 52.3 30.705 68.64 104 5.4 13.49 27 3.58 1.6 1502.5 419.5 B IV 02 19 36 43.6 30.835 65.27 179 5.4 14.46 349 3.61 3.1 1616.6 447.9 C 7-74 VIII 14 17 56 48.3 32.285 69.11 141 5.3 16.24 3 3.61 9.5 1803.9 501.3 C 8-74 'II 16 07 47 51.5 33.345 68.33 35 4.8 16.47 1 3.54 C.6 186C.3 525.5 B 9-74 VIII 17 12 12 45.2 11.889 64.41 47 4.7 7.21 331 3.63 3.8 882-5 221.1 B 10~74 VIII 24 19 58 28.8 31.365 67.40 12 5.3 14.77 357 3.52 2.5 1641.1 466.2 8 11-74 VIII 27 15 20 58.4 27.875 66.70 149 5.5 11.36 353 3.53 3.5 1271.9 359.6 B 12-74 1X 03 28 22 28.5 25.895 67.64 45 4.8 9.30 357 3.48 6.8 1034.3 297.5 C 13-74 X 96 87 47 51.5 38.935 65.89 48 4.7 14.68 348 ----- 1622.7 ----14~75 V 06 18 10 02.0 32.935 63.02 14 5.0 16.35 3 3.53 2.0 1816.7 505.0 8 15-75 V 18 02 40 22.8 23.905 66.00 3 --- 7.60 344 3.55 1.1 844.4 238.8 C 16-75 VI 05 14 32 11.8 23.019 65.52 173 4.7 11.52 352 3.57 3.9 1291.6 361.8 B IX 85 19 10 9.2 24.005 66.7! 192 4.9 7.62 350 3.50 6.3 366.1 240.8 8

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IX 20 21 07 02.0 32.595 68.70 24 4.9 16.00 2 3.50 1.0 1777.9 508.0 8
18-75
19-75 XI 17 06 45 46.0 31.63$ 69,40 112 5.2 15.07 5 3.55 1.4 1678.2 473.0 B
28-75 XII 86 85 35 37.8 38.895 68.85 122 5.8 14.31 3 3.61 3.8 1594.6 441.7 C
21-76
        I 04 04 42 4.0 27.905 66.00 128 4.8 11.47 350 3.52 0.8 1280.8 364.0
22-76
       II 14 89 81 52.8 33.655 68.92 28 4.8 17.86 3 3.53 8.9 1895.6 537.8
23-76 III 20 02 55 47.8 27.365 67.36 118 4.8 11.02 356 3.57 0.8 1230.1 344.2 C
24-76 III 27 21 05 7.1 31.83$ 67.66 122 5.1 15.24 358 3.55 0.1 1687.7 478.9 C
        V 04 02 07 11.3 27.305 65.80 58 4.7 10.56 348 3.39 3.2 1219.1 359.6 C
26-76 VIII 03 23 43 54.6 31.535 68.49 119 5.0 14.94 2 3.70 2.3 1660.0 449.4
27-76
     IX 12 03 51 24.5 24.14S 66.78 178 4.8 7.67 351 3.60 0.4 870.6 241.5
28-76
       X 24 00 13 51.0 32.805 69.20 25 4.9 16.23 4 3.53 1.6 1803.5 511.0 C
29-76
      Y' 25 07 13 38.0 27.985 64.73 25 5.0 11.81 344 3.51 1.8 1312.4 374.0 C
36-76
          _5 14 49 58.8 29.665 68.90 140 5.0 13.09 4 3.61 2.1 1461.2 404.3 C
31-77
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32-77
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      VI 27 22 53 57.0 30.395 67.10 52 4.8 13.83 356 3.52 9.0 1537.5 436.8 C
34-77 VIII 03 14 27 32.5 31.675 69.29 51 5.0 15.11 4 3.49 0.2 1679.6 481.3 C
35-77 VIII 29 16 36 1.9 31.905 69.22 114 5.3 15.33 4 3.62 3.8 1707.1 471.6 C
36-77
       XI 23 89 26 23.4 31.845 67.76 4 6.4 14.45 359 3.62 4.9 1605.5 443.6 B
37-77
       XI 23 11 08 43.0 31.328 67.82 32 5.3 14.72 359 3.67 0.8 1635.8 446.0
38-77
       XI 23 11 44 23.8 31.60S 67.85 60 4.7 15.00 359 3.61 0.5 1667.7 462.0
39-77
      XI 23 11 46 55.4 31.835 67.58 8 5.2 14.44 358 3.62 1.9 1684.4 443.6 C
     XI 23 11 58 10.0 31.005 67.86 22 5.5 14.40 359 3.67 3.2 1600.1 444.5 C
41-77
     XI 23 13 38 51.0 31.485 58.20 49 4.8 14.88 8 3.52 8.4 1654.8 470.8 C
42-77
      XI 23 13 50 38.0 31.365 68.00 78 4.9 14.76 359 3.64 1.0 1641.8 451.0
43-77
      XI 23 15 37 56.0 31.805 67.74 65 4.6 15.20 359 3.53 0.3 1688.8 478.4
44-77
      XI 23 16 17 51.0 31.215 67.52 20 4.5 14.62 358 3.59 1.2 1624.0 452.4 C
45-77
      XI 23 16 28 23.9 31.265 67.65 10 5.1 14.76 358 3.70 2.7 1638.9 448.8 B
46-77 XI 23 16 36 3.0 31.30S 67.73 21 5.6 14.70 359 3.54 5.3 1633.4 461.4 C
47-77
       XI 23 16 40 53.1 30.805 67.10 33 5.1 14.23 356 3.56 3.0 1581.4 443.0
48-77
       XI 23 21 52 2.5 31.43$ 67.71 36 4.9 14 4 359 3.53 1.2 1648.2 467.5 C
49-77
      XI 23 21 57 28.3 31.685 67.74 62 4.8 15.08 359 3.43 0.6 1676.7 488,7 €
50-77
      XI 23 23 04 13.4 31.825 67.98 84 5.0 15.22 359 3.43 0.6 1693.2 493.6 C
51-77
      XI 23 23 27 36.8 31.315 67.69 20 5.1 15.02 358 3.45 2.1 1668.9 484.0 C
52-77
       XI 23 23 32 28.8 38.375 67.37 23 --- 13.79 357 3.56 1.1 1532.4 438.8 B
53-77
       XI 24 88 88 29.1 31.885 67.53 33 --- 15.21 358 3.59 2.1 1698.3 469.9
                                                                           C
54-77
       XI 24 03 20 05,6 31.71S 67.80 62 4.4 15.12 359 3.54 1.7 1181.1 475.0 C
55-77
       XI 24 83 57 50.0 31.798 67.80 48 4.3 15.19 359 3,60 0.8 1688.4 468.0 C
56-77
       XI 24 84 59 27.8 31.925 67.68 62 --- 15.31 358 3.38 8.4 1782.2 583.8 C
57-77
       XI 24 '5 86 24.9 31.755 67.68 45 4.3 15.16 358 3.55 2.5 1685.8 475.1 C
58-77
       XI 24 95 13 35.8 31.645 67.61 19 4.2 15.95 358 3.43 9.8 1672.2 487.5
59-77
       XI 24 11 98 39.9 31.705 67.90 83 4.0 15.10 359 3.44 0.5 1677.8 488.8 C
68-77
       XI 24 18 28 16.5 31.315 67.69 33 5.6 14.72 358 3.48 1.2 1635.5 481.8 C
61-77
       XI 24 18 42 40.0 31.375 69,79 26 5.8 14.77 359 3.62 2.8 1641.3 453.4 C
       XI 24 22 19 58.3 31.485 67.76 51 4.4 14.88 359 3.61 0.3 1654.1 457.7 C
62-77
63-77
       XI 24 23 88 54.5 31.245 67.76 47 4.9 14.65 359 3.58 1.9 1628.4 465.5 C
64-77
       XI 25 08 04 31.6 31.065 67.73 43 5.4 14.47 359 3.48 8.6 1608.3 462.4 C
65-77
       XI 25 83 24 37.3 31.675 67.25 33 4.5 15.88 359 3.63 4.2 1675.8 461.7 C
66-77
       XI 25 83 47 16.6 31.795 67.75 41 5.8 15.19 358 3.62 3.4 1688.2 466.4 C
67-77
       XI 25 84 86 53.1 31.195 67.78 22 4.8 14.59 358 3.63 2.8 1621.2 445.9 C
       XI 25 18 02 40.3 31.245 67.82 53 4.9 14.69 359 ----- 1632.5 ----
68-77
69-77 XI 25 18 56 32.1 31.365 67.48 33 4.9 14.78 358 ----- 1642.8 ----
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78-77
        XI 25 28 42 15.6 31.385 67.53 47 4.1 14.70 358 3.34 1.2 1633.8 210.2 C
        XI 26-00 44 9.0 31.615-67.65 24 4.7 15.02 358 3.45 0.8 1669.0 484.0 C
 71-77
 72-77
        XI 26 13 52 21.5 31.345 67.49 33 5.8 14.75 358 3.65 8.7 1639.2 448.5 C
 73-77
        XI 26 20 26 51.0 31.355 67.70 33 3.7 14.76 358 3.54 1.0 1640.3 463.0
 74-77
        XI 27 86 26 4.8 31.135 67.78 33 3.6 14.54 358 3.59 8.2 1615.9 458.8
 75-77
        XI 27 20 15 5.3 31.655 67.80 47 4.8 15.05 357 3.59 1.1 1672.9 464.7 C
 76-77
        XI 23 88 17 24.3 31.895 67.68 28 5.3 14.41 358 3.59 1.5 1681.3 445.7
 77-77
        XI 28 04 19 31.0 31.685 67.65 2 5.6 15.88 358 3.54 11.1 1675.5 473.0
 78-77
        XI 28 85 39 24.0 38.975 68.85 23 5.3 14.37 368 3.55 7.4 1596.8 458.8
        XI 28 06 31 29.1 31.445 67.44 17 5.9 14.85 358 3.58 14.3 1658.1 468.9 B
 79-77
 88-77
        XI 28 18 40 18.8 31.905 69.01 97 5.2 15.32 3 3.66 1.1 1705.0 466.2 C
        XI 28 23 87 57.0 31.698 67.30 1 4.9 15.10 357 3.32 3.0 1677.8 477.8 C
 R1-77
        XI 29 00 33 38.9 31.625 67.80 33 4.8 15.03 359 3.53 6.5 1670.3 473.0 B
 83-77 XII 85 15 43 26.6 31.105 67.96 11 5.4 14.56 359 3.55 3.0 1611.1 453.8 C
 84-77 XII 06 08 41 35.8 31.025 67.74 5 5.4 14.43 359 3.53 5.2 1603.3 454.2 B
 85-77 XII 06 17 85 6.9 31.245 67.90 21 5.9 14.64 359 3.56 7.8 1626.8 457.1 B
 86-77 XII 06 18 27 38.0 31.305 67.63 4 5.1 14.71 358 3.46 0.6 1634.4 472.4 C
 87-77 XII 87 88 32 36.2 28.635 67.38 128 5.3 12.86 347 3.61 1.5 1646.1 372.8 B
 88-77 XII 07 03 22 44.0 31.195 67.88 27 5.1 14.59 359 3.56 6.5 1621.3 456.0 C
 89-77 XII 09 21 44 50.0 31.585 67.85 14 4.9 14.98 359 3.59 1.5 1664.5 463.8 C
 98-77 XII 18 87 11 55.6 31.275 67.78 39 5.1 14.67 358 3.45 9.5 1638.4 472.6 C
 91-77 XII 10 08 37 1.0 31.275 67.75 37 4.8 14.65 357 3.56 3.7 1628.0 457.3 B
 92-77 XII 10 14 19 57.9 31.215 67.75 27 5.2 14.62 359 3.44 1.4 1624.6 372.1 C
 93-77 XII 12 16 02 33.0 31.385 67.50 40 4.9 14.79 358 3.40 0.9 1643.8 483.0 C
 94-77 XII 21 03 47 32.2 31.585 67.70 33 5.7 14.98 359 3.65 5.8 1664.7 455.8 C
 95-78
         1 01 10 50 56.0 31.145 69.88 17 5.1 14.54 359 3.52 2.9 1615.6 459.0 C
 36-78
         I 03 01 10 4.4 31.545 67.90 35 5.3 14.94 359 3.67 1.3 1660.4 452.6
 97-78
         I 03 06 31 5.1 31.265 67.83 38 5.0 14.67 359 3.69 1.2 1630.4 441.9 C
 98-78
         1 17 11 33 14.5 21.255 68.00 20 5.8 14.65 360 3.65 15.2 1627.9 445.5
 99-78
         1 22 12 08 25.8 31.455 67.97 35 4.6 14.85 359 3.39 0.7 1650.3 459.2 C
190-78
         I 24 13 18 15.7 31.748 68.91 18 5.6 15.15 3 3.64 2.2 1683.4 462.3 C
101-78 111 18 00 38 40.0 31.415 67.80 16 5.1 14.81 359 ------ 1645.6 ----
102-78
        IV 04 19 33 53.3 31.205 67.74 17 5.4 14.60 359 3.61 2.8 1622.3 449.4 C
103-78
         V 10 23 06 02.0 29.975 67.91 3° 5.1 13.40 3 3.66 2.2 1489.3 407.0 C
104-78
        VI 07 15 16 45.0 32.085 67.56 44 5.1 15.49 358 3.41 6.5 1721.6 505.0 C
195-78
       VI 26 18 49 11.8 31.605 67.71
                                     0 5.1 15.01 359 3.52 0.5 1667.3 473.2 C
106-78 VII 26 01 47 16.1 31.345 67.76 46 5.0 14.94 359 3.53 0.9 1660.6 469.9 C
107-78 VIII 21 00 28 25.1 31.285 67.86 25 5.5 14.68 359 3.61 2.4 1636.3 453.7 C
108-78
         X ~ 01 36 41.7 31.545 67.68 43 5.3 14.95 358 3.61 1.1 1661.6 468.3 C
189-79
         1 29 93 22 45.5 31.268 68.49 19 5.9 14.66 1 3.62 9.7 1628.3 450.9
118-79
        11 23 23 08 3.1 31,155 68.34 51 4.8 14.56 1 3.69 8.9 1618.5 438.6
111-79 VIII 38 18 59 46.9 31.475 67.69 47 5.4 14.88 358 3.72 9.8 1654.8 443.1 C
112-79
         X 98 01 52 48.0 31.465 68.04 39 4.8 14.86 360 3.64 4.0 1651.6 453.7 8
113-88
         I 17 11 80 10.0 31.475 67.70 29 4.8 14.88 359 3.52 8.1 1653.6 470.0 C
114-88
         1 24 18 34 4.1 31.798 63.50 43 4.7 15.19
                                                  1 3.51 9.9 1689.3 489.9
                                                                           1
115-09
        IV 09 08 17 57.4 31.658 67.48 23 5.4 15.06 358 3.54 8.1 1673.5 472.6 C
         V 25 21 46 11.8 31.335 68.00 43 5.0 14.73 360 3.53 1.5 1637.2 463.2 C
116-88
        XI 10 16 24 39.0 31.625 67.47 13 5.6 15.03 358 3.61 2.6 1670.0 463.0 C
118-90 XII 06 03 43 11.5 31.265 67.52 46 4.8 14.67 359 3.58 1.7 LELY.S 455.5 C
119-Bi VII 02 11 03 35.0 32.995 69.88 58 4.5 16.41 3 3.58 0.7 1824.2 589.8 C
121-82 XII 84 03 26 42.6 31.275 67.75 36 4.9 14.67 359 3.59 1.2 1638.4 453.4 B
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122-83 XI 26 17 80 2.1 31.485 68.88 108 5.1 14.89 3 3.63 8.8 1657.9 448.0 C 123-83 XII 84 82 80 35.4 31.775 69.42 113 5.2 15.21 5 3.51 3.7 1693.7 492.5 B 124-83 XII 84 82 99 20.8 24.855 66.79 191 5.2 7.57 358 3.63 2.7 862.5 237.6 B 125-86 III 12 22 84 19.1 24.885 66.80 198 5.2 7.69 351 3.47 8.6 877.1 252.9 B
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CHILE

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1-72
        V 15 09 12 56.6 29.705 71.30 49 4.9 13.40 13 3.52 5.9 1489.7 423.4 C
 2-72
        V 15 10 09 38.0 29.605 69.40 17 5.4 13.09 6 3.66 14.1 1454.5 397.0 B
 3-72
        V 28 07 28 13.5 27.705 71.30 53 4.8 11.47 15 3.65 25.1 1275.5 348.5 8
        V 28 09 46 14.5 27.705 71.40
 4-72
                                    4 4.9 11.48 16 3.66 19.3 1275.5 348.5
 5-74
        I 86 86 28 15.2 29.885 71.26 67 5.8 13.52 13 3.61 5.8 1537.8 416.8 C
 6-74
        I 06 15 01 34.5 23.775 68.79 87 5.3 7.23
                                                 5 3.58 13.6 808.0 225.5 B
 7-74 VIII 04 21 08 52.8 24.455 69.94 66 5.0 8.07 13 3.52 5.6 899.1 255.0 B
 8-74 VIII 03 17 17 1.6 37.235 73.62 11 5.0 21.19 15 3.59 0.7 2354.4 355.4 C
9-74 VIII 15 18 27 30.6 18.005 71.03 38 5.4 18.75
                                                 9 3.61 1.1 2085.6 577.4
10-74 VIII 17 14 38 38.6 19.295 69.74 98 4.2 3.15 30 3.45 0.3 363.3 105.4
11-74 VIII 18 10 44 11.8 38.345 73.27 19 5.9 22.20 13 3.60 10.7 2466.7 684.0 C
12-74 VIII 24 04 16 26.2 22.605 68.70 101 5.3 6.05
                                                6 3.62 2.6 680.8 197.8 B
13-74 VIII 27 05 24 6.5 38,295 73.53 15 5.4 22.20 14 3.56 1.1 2466.7 692.5 C
14-74
      1x 04 03 40 37.0 18.005 71.30 46 4.0 3.41 65 3.44 2.2 381.7 111.0
15-74
       IX 20 04 48 35.7 19.805 69.35 116 4.6 3.46 20 3.51 2.1 401.6 114.3 C
16-75
        I 81 22 31 5.8 38.335 73.24 24 5.3 22.18 13 3.58 8.1 2464.5 688.8 C
17-75
        I 02 21 35 18.1 32.335 70.07 112 5.1 16.65 7 3.6% 1.7 1853.4 514.8 C
18-75
        I 04 15 02 41.5 32.465 71.42 77 4.3 16.14 12 3.73 2.5 1794.9 480.5 C
19-75 III 05 28 29 41.1 28.525 68.77 108 4.7 4.01
                                                9 3.59 6.0 458.4 127.6 B
28-75
       VI 18 23 88 46.8 22.535 68.78 151 4.8 6.88
                                                 6 3.52 0.6 683.3 194.0 B
21-75
       VI 14 18 40 28.3 32.525 78.68 92 5.6 16.80 9 3.57 38.4 1788.1 497.7 8
22-75
       VI 15 10 45 9.2 22.595 68.40 100 --- 6.03
                                                 3 3.67 2.7 678.6 184.8 C
23-75
       VI 22 22 53 5.3 22.395 68.30 137 5.1 5.83
                                                  2 3.68 8.4 662.1 179.9 B
24-75 VII 24 06 42 35.0 33.055 70.15 162 4.6 16.55
                                                  7 3.41 0.3 1841.7 540.1 C
25-76
       II 81 89 45 24.8 19.315 78.49 33 --- 3.58 48 3.58 8.2 399.1 114.8 C
26-76
      VI 14 07 53 8.4 22.345 70.10 33 --- 6.07 18 3.50 5.4 675.2 192.6 C
27-76 VIII 84 84 17 27.8 25.24S 63.23 91 4.7 8.73
                                                 7 3.57 3.2 974.2 273.0 B
28-76 XII 82 88 89 11.4 28.645 69.88 176 --- 4.38 21 3.68 2.9 517.5 143.6 C
29-76 XII 82 87 31 16.4 38.515 71.28 43 5.8 12.28 14 3.44 2.1 1365.1 396.6 C
38-77
        I 25 86 11 2.9 25.598 78.26 48 4.8 7.31 17 3.64 2.8 813.2 223.1 B
31-77
       IX 03 20 12 38.5 22.59S 68.59 126 4.8 6.04
                                                4 3.56 4.8 £82.8 191.8 C
32-77
       IX 17 22 39 51.8 28.385 68.91 33 --- 3.83 12 3.65 5.5 426.8 185.8 C
33-77
       XI 24 17 57 29.8 21.815 67.62 188 4.8 4.48 354 3.67 2.7 532.1 145.1 C
34-77
       XI 27-85 51 22.9 28.835 78.38 75--- 4.85 31 3.53 828 456,2 129,8 C
35-77
       XI 28 09 13 39.8 28.285 69.05 117 4.3 3.92 18 3.50 8.5 458.9 129.5 B
36-77
      XI 27 22 58 42.4 21.655 68.52 119 4.9 5.11 5 3.59 4.9 588.1 161.6 C
37-78 III 15 01 09 23.5 21.435 69.20 172 --- 4.49 12 3.68 5.0 527.7 146.5 B
38-78 VII 25 21 57 57.1 20.645 69.80 148 --- 4.18 12 3.32 1.1 487.4 146.9 C
39-79
       IV 19 02 59 45.3 24.215 67.28 190 --- 7.67 354 3.51 0.8 842.2 248.7 C
48-79
      IV 19 07 16 45.6 40.285 71.90 33 4.5 23.89 9 ----- 2654.6 ----
41-79 VIII 38 89 15 50.2 21.215 68.60 118 5.4 4.68 5 3.56 2.6 533.2 149.8 C
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IX 82 14 29 38.5 20.665 68.74 110 5.0 4.15 9 3.58 35.7 474.0 132.5 B
43-88
       XI 98 21 35 42.3 24.425 67.67 98 5.3 7.86 357 3.59 5.6 878.8 244.7 B
      XI 25 06 04 2.9 34.835 70.88 34 5.0 18.37 8 3.63 1.0 2043.2 563.1 C
45-81 XII 08 22 05 45.0 22.325 68.92 118 5.0 5.18 8 3.37 4.7 587.5 174.0 C
46-81 XII 09 04 34 48.5 20.745 69.37 114 4.5 4.35 16 3.46 4.8 496.6 143.5 C
        X 23 15 37 7.5 19.775 69.48 143 --- 3.46 22 3.64 4.4 410.2 112.7 B
        X 23 16 02 29.9 20.285 70.50 34 4.8 1.36 31 3.67 3.2 485.6 132.3
48-82
        X 26 03 24 30.1 29.705 71.40 63 5.6 13.44 14 3.65 2.6 1494.5 409.3 B
50-83 III 05 22 10 29.4 29.325 71.70 35 5.2 13.15 15 3.37 3.1 1431.5 435.5 C
51-83 111 31 17 32 58.8 21.455 68.81 167 5.1 4.94 8 3.52 5.3
52-83
        V 03 05 55 21.6 22.805 68.12 144 4.6 6.32 8 3.47 7.1 716.8 206.4 ?
53-83 VII 05 16 48 6.6 24.035 67.05 183 4.8 7.53 352 3.54 1.1 856.4 241.6 C
54-83 VII 06 05 54 55.8 24.175 67.09 189 4.4 7.65 353 3.64 0.5 849.1 233.2 C
55-83 VII 97 04 50 37.8 28.69S 58.96 112 4.9 4.21 11 3.53 2.5 480.9 136.2 C
56-83 VII 08 02 03 16.0 20.705 69.50 82 5.2 3.76 21 3.68 0.8 425.7 115.7 C
57-83 VII 15 23 41 9.5 23.105 68.20 172 --- 6.56 1 3.59 2.1 748.9 208.5 C
58-83 VII 19 04 33 24.5 22.665 68.49 126 4.7 5.51 4 3.62 4.8 625.0 172.5 C
59-83 VII 19 20 21 28.8 24.235 67.07 192 4.3 7.72 352 3.57 0.4 678.9 246.5 C
60-83 VII 19 22 10 39.3 20.655 69.50 158 --- 4.30 18 3.60 1.4 523.2 133.7 C
61-83 VII 20 05 40 52.5 22.80$ 68.85 128 4.7 6.28 7 3.63 5.5 705.4 195.5 C
62-83 VII 20 22 11 54,0 25,375 70,20 69 --- 9.01 13 3,60 1.6 1003.5 278,6 C
63-83 Vil 11 97 11 13.3 22.345 68.54 119 5.5 5.79 4 3.60 4.7 654.2 181.7 C
64-83 XII 01 16 29 44.0 26.335 71.00 49 4.5 10.11 16 3.58 0.8 1124.4 314.2 C
65-83 XII 03 21 45 1.3 24.219 67.10 198 --- 7.70 353 3.55 8.5 878.1 247.0 C
66-83 XII 14 07 38 58.0 25.885 71.20 35 4.3 9.73 18 3.51 2.1 1081.7 308.2 C
67-83 XII 15 84 22 33.9 33.898 70.15 103 5.9 16.59 7 3.56 2.6 1846.2 538.1 B
68-83 XII 16 02 40 5.9 21.635 68.42 123 4.9 5.08 3 3.58 7.7 577.5 161.0 B
69-83 XII 23 86 45 31.5 19.42S 69.29 124 4.4 3.89 22 3.58 1.3 136.5 181.8 B
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71-83 XII 23 22 56 7.1 27.485 71.41 33 5.0 11.31 16 3.53 2, 1257.1 356.1 C
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Characteristics of Lg

Short period waves of apparent velocity around 3.5 km/s, transversely polarized are considered here (exclusive of faster Li and slower Rg, though other authors consider those together with $L_{\rm g}$).

In South America Lg originates in most of earthquakes not deeper than 200 km and are transmitted by continental crust, mostly by ancient stable zones.

The velocity for the beginning of the waves in most cases may not be measured precisely, because of its emerging character. We considered the apparent group velocity, that is to say, the ratio of hypocentral distance to the time between origin and initial Lg recording (without any distinction of time for waves before being confined within a guide layer and the time travel along that layer). That apparent velocity was found to change between 3.44 and 3.69 km/s (coincident with the S-wave velocity within the crust).

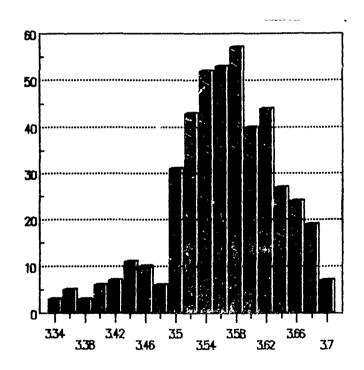


Fig. 1 .- Lg apparent velocity (km/s).

The amplitude is a function of magnitude, epicentral distance and local conditions both of generation and transmission. To

normalize a measure avoiding any effects of distance and magnitude, we calculate Lg amplitude/P amplitude; this ratio changes between 0 and 17, with an exceptional case of 38.

Bath (1954), with the same goal of normalization, suggests a relative measure of wave energy that we shall name here by the symbol e. He acknowledges some inconsistencies of results, as we acknowledge for Lg/P; so we shall use both ways of normalization.

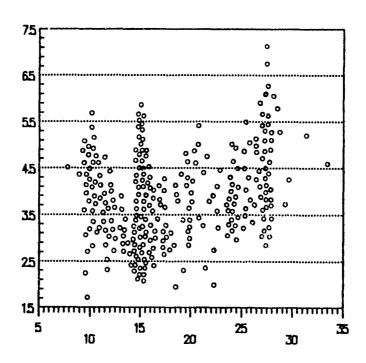
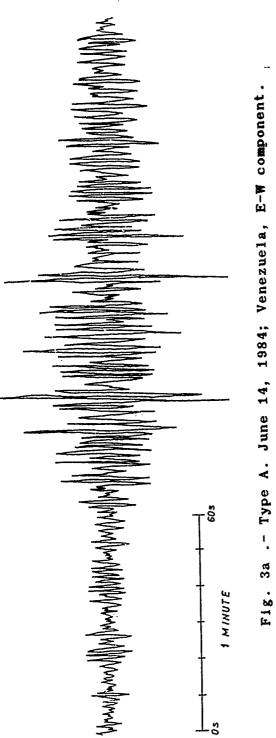


Fig. 2 .- Normalized energy vs. epicentral distance.

According to the transmission efficiency and the aspect of Lg (fig. 3), we distinguish:

- Type A: Clear waves, well developed, beginning almost always impulsive.
- Type B: Clear waves interfered by low frequency waves, emergent beginning (exceptionally impulsive), starting with medium amplitude to decrease then gradually.
- Type C: Waves not clear, disturbed by noise, emergent or really doubtful beginning, small but rather constant amplitude.

Often Lg splits into several phases, that means several arrivals at different velocity and amplitude but coincident for the other aspects (until the moment it is not possible to decide if they have traveled along different layers, or the whole crust



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Fig. 3b .- Type B. November 26, 1984; Colombia, E-W component.

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Fig. 3c .- Type C. November 18, 1988; Argentina, E-W component

is the guide for Lg1 and the most superficial layer guides Lg2).

The lack of uniformity in wave relevance is the main characteristic of South America, recommending by itself to forget any possibility of considering it instrumental for magnitude measurements.

Let us consider different measures for the different seismogenic regions:

Venezuela, Trinidad and Southern Caribbean

Types A and B are predominant. Lg lasts about two minutes, generally disappearing below Love and Rayleigh waves. The mean velocity amounts $3.58\pm.603$ km/s. Several arrivals, even four, are common.

Mean amplitude Lg/P is $4.5\pm.395$, being differences of regional character; e is $4.45\pm.129$.

In the eastern part of that region focal depth may reach 144 km, that means the Caribbean plate subduction. Western earthquakes around Lake Maracaibo all are shallower than 75 km.

Colombia

The three types, A, B, C, are found in Colombia. Mean apparent velocity is $3.57\pm.006$ km/s. Amplitude changes so much that the mean $2.77\pm.294$ is of little interest. For earthquakes deeper than normal Lg lasts two and a half minutes.

We need to distinguish three zones: The Lg from the West Coast and Western Cordillera is much attenuated at LPB and type C is predominant. For the Central Cordillera type B predominates. In the most eastern stripe (subandean to flat lands) type A prevails and several phases are apparent.

The seismic nest of Bucaramanga is a point of special interest: earthquakes occur at 125 to 175 km depth (only one exception of depth 59 km was found), meanwhile in the rest of Colombia only four other earthquakes occurred deeper than 81 km.

Other phases: S only was visible in 36 cases among 52; Rg only in several surface earthquakes which had Lg type A; in general other phases are much attenuated.

Ecuador

Type C is predominant. Small amplitude $1.52\pm.245$ as an average, but larger $e=3.89\pm.138$. Several distinct phases of Lg, specially for intermediate depth feei, the faster one with a mean velocity 3.58+.995km/s.

Earthquakes originate partly near the coast at a depth less than 55 km; the others at the subduction zone are deeper, reaching 182 km.

Rg hardly is visible; several phases in between P and Lg are more relevant than for Venezuela and Colombia earthquakes.

Brazil

Deep earthquakes from Western Brazil were not taken into account after realizing that they do not generate any Lg. The other Brazilian earthquakes occur all at the crust (unless one calculation at 63 km be correct).

The path of Lg is mostly through Brazil and Guyana Shields, with an apparent velocity $3.58\pm.007$ km/s; so Lg is well developed, type A, with a mean amplitude Lg/P $5.2\pm.245$ and e $4.53\pm.188$.

P and other seismic phases are clear.

Peru and Peru-Brazil Border

Type A predominates, independently of distance. Focal depth between \emptyset and 198 km. Superposition of Love and Rayleigh waves disturbes the final Lg. Mean apparent velocity is $3.56\pm.003$ km/s; mean $e=4.9\pm.109$. Approximate duration of Lg one minute.

In most cases two or more phases are clear within the Lg.

Chile

North Chile earthquakes occur at less than 10 degrees of distance to LPB, making difficult or also uncertain Lg analysis.

Type C predominates for any depth (ranging from 4 to 198 km). Apparent velocity may change from 3.35 to 3.69 km/s. As a general rule wave period is longer than for other azimuths, what is important to be remarked, since for this range of wave period instrumental gain is low, so that at a first glance Lg amplitude is minimum and, when measuring it, we find Lg/P $4.75\pm.255$; e 3.21 $\pm.124$ but P attenuation is strong, what allows a calculation larger for Lg/P. Lg always is a simple phase, meanwhile a double P appears for intermediate depth earthquakes (not for surface earthquakes).

Argentina

Most of the earthquakes are superficial, but several at the Nazca plate subduction are deeper, reaching 198 km, all being of type C. Lg apparent velocity is low, averaging $3.56\pm.005$ km/s. Lg/P is $2.4\pm.225$; e is $3.1\pm.07$. Three to five seconds after first P arrival, another phase is relevant; on the contrary Lg is always simple. Length of period is rather large (the same as remarked for Chilean earthquakes).

Lg both for Argentina and Chile has a short duration or it does not appear at all; often it emerges on the S coda. It is not clear why some earthquakes produce Lg and other with identical apparent circumstances do not.

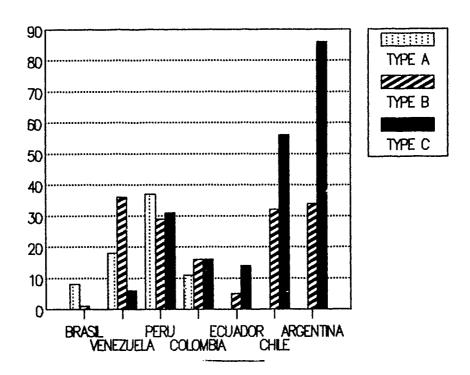


Fig. 4 .- Comparison of Lg types of recording in LPB, acording to origin regions.

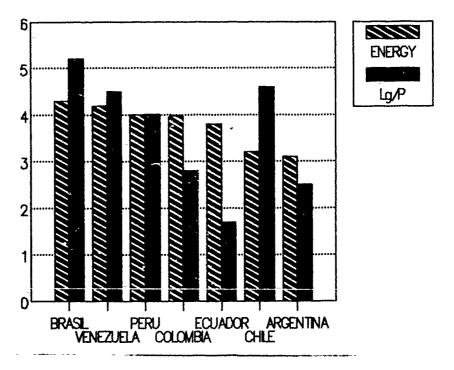


Fig. 5 .- Normalized wave energy and Lg/P amplitude.

Lg according to path characteristics

Amplitude and type of Lg depends more on the wave path than on the origin conditions.

Propagation of Lg along ancient stable structures is really efficient; at the other end, 200 km of oceanic path extinguishes completely Lg. The complex cordilleran structures have been considered inefficient paths; nonetheless the analysis of LPB records only gives a partial confirmation. Let us see this matter with more detail.

The earthquakes originated in Brazil and Venezuela have most of their path across Brazilian and Guyana Shields and they show large Lg at LPB.

Records of Chilean and Argentinian earthquakes have smaller or no Lg, being their path along cordileran structures (but our measures give stronger Lg, mainly for longer periods, because also P is small).

Western Colombia earthquakes need to undercross the Cauca Graben. This, according to some authors, means a line of contact of an ancient subduction; others interpret it as a contact of obduction; any way it is considered a plate discontinuity which may difficult Lg crossing. Moreover magmatic chambers may constitute obstacles to Lg. Earthquakes from the eastern side of Cauca Graben produce a clearer Lg in La Paz. Again foci in the most eastern seismogenic Colombia have a relevant Lg in LPB records.

The path from Peru and Peru-Brazil Border proves to be of medium efficiency: Lg waves are rather large, with several arrivals, but last only a short time. Such complex path merits a deeper analysis.

Many intermediate depth earthquakes produce remarkable Lg in South America, against the hypothesis that Lg originates always at surficial layers; probably the efficiency in Lg generation depends on the strike of subduction.

Geological crustal profiles for different paths across South America may be seen in Alcócer (1989), Ayala (1989), Couch et al. (1981), Meissner et al. (1976).

PART II. Lg RECORDED IN SEVERAL SOUTH AMERICAN STATIONS

After considering with detail Lg propagated through South America, recorded at LPB station, now it is much easier to revise Lg in other stations belonging to the World-Wide Seismograph System Network, and to show numerical results of our analysis. We have tried to make that analysis the most objective possible, studying the same earthquakes, by using stations similar to LPB and applying the same criteria as in part I. See table II (similar to table I).

TABLE II

ï		DAT	Ε		H		LAT	LON6	W P	a b	D	Az	V	Lg/	P D	t	Amp	Ţ	e	ſ
	<i>y</i>	; <u>a</u>	ل	h	Æ	S	(0)	(5)	(ka)	(6)	(0)	(ka/s	()	(km)	(5)	(alf)	(5)		
										c	OLOMBI	<u>A</u>								
PB	5 ₹	VIII	88	82	58	36.2	7.02N	72.11	39	5.8	23.73	178	3.56	8.3	2636.9	738.8	649.8	1.5	5.3	9
NT																938,8				
RE																744.6				
NA D6																607.3 93.8				
ua											3.61	£17	2.00	219	343.3	33.0	/44.0	1.0	4.0	٥
e B	88	11	18	16	34	38.5	6.82N	72.92	171	4.9	23.68	168	3.53	1,8	2635.6	746.5	38.8	8.8	3.5	5
₹E																711.5				
ĄŔ											5.97	58	3.66	1.5	793.1	216.5	246.0	1.0	4.1	٥
 PB	91	VIII	 95	12	 58	28.8	3,98%	76.39	62	5.1	21.92	158	3.56	1.9	2436.3	685.0	88.9	1.8	3.6	8
₹E																675.7				
IA																582.8				
J6																537.8				
RN											21.20	136	3.38	1./	2454.1	521.2	13/.5	1.3	J. /	
	82	VIII	15	87	26	28.3	6.74N	73.01	172	4.9						739 7				
NA.																271.7				
EL Rn																1201.7 331.9				
											12.12	70	0,00	0.0	101010	00117	03,0	0.)	J.7.	•
	33-	VIII	29	8	24	24.7	6.8 0 N	73.00	169	5.8						721.3				
RE IA											19.88				2576.2	615.3	215.0			
16																432.7				
										VE	NEZUELI	Ī								
B	76	XII	21	84	32	31.8	8.8 0 N	61.78	48	4.7						783.8 831.1				
iÿ iç																774.0				
N.					N	IO Lg					1.90				214.9					•

LPB Nna	77	XII	17	23	25	18.5	18.90	65.	50 14	4.6					3042.2 2821.1					
rn															443.5					
LPB NNA										4.6	27.28	193	3.54	6.6	3888.2 2935.9	847.2	247.5	1.5	5.38	
J6 RN					1	KG Lg						335	3.56	2.9	966.4	271.2				
•			-					*****	a b	AR	GENTIN	<u> </u>	p = 10 pr = 11				, , , , , , , , , , , , , , , , , , ,			
L?B	74	VIII	17												892,5					
NT															521.3					
RE 106															1926.6 3213.3					
INA															1783.9					
IUI															2931.5					
	74	IX	0 3	28	22	26.5	25.899	67.	64 45						1934.3					
ARE ANT															1117.6 373.8					
 .PB	 76	 V	1 4	8 2	87	11.3	27.309						-		1219.1			1.4	3.55	 C
ANT															617.2					
RE Na															1249.1 2051.9					
EL														-	825.4					
							33.599	68.	27 28	5.4	16.98	1	3.54	5.9	1805.7	533.8				
INT IRE															1114.6					
106															1922.3 4265.5					
.PA															909.1					
IŃA															2542.3				2.57	¢
LPB NÁ		XI	26	13	52	21.5	31.349	67.4	19 33	5.8					1639.2 2345.8					

																		22.5			
INT		•						•		•								89.9			
RE																		15.9			
306																		24.0			
CAR																		15.3			
HK												41.00	78	3,00	1.0	4022.4	1769.7	10.5	6.7	3.0	ם
 PB	 83	TII	84	B 2	 86	35.4	 31.7	 75	69.42	113	5.2							98.0			
NT																		100.0			
AR																		85.2			
NA																		35.0			
											!	CHILE									
PB	72	٧	15	1 9	12	56.6	29.7	85	71.38	49	4.9	13.48	13	3.52	5.9	1489.7	423.4	112.8	1.4	3.6	8
RE	-	•			_													234.0			
EL																		135.1			
PB	 72	V	28	97	28	13.5	27.7	85	71.38	53	4.8	11.47	15	3.66	16.3	1275.5	348.5	213.0	1.7	4.1	4
RE												11.16	359	3.56	4.3	1248.7	348.8	256 .6	1.8	4.7	4
06												32.22	355	3.58	1.1	3580.2	1000.2	42.8	8.6	4.4	2
AR												38.18	7	3.67	1.3	4242.4	1155.5	146.9	1.8	4.7	8
PA												13.49	126	3.69	7.7	1499.4	406.5	864.0	1.4	5.6	4
DD	 75																	420.0			
NT	,,	**	47		70	20.0	72.0		70.00	14								992.5			
RE																		110.5			
06																		168.8			
PA																		367.2			
17												10.07	100	3,00	2.0	121010	43717	00/12		5. 7	•
PB	82	X	 26	1 3	24	30.1	29.7	us.	71.48	63	5.6	13.44	14	3,65	2.6	1494.6	499.9	237.5	1.1	3.2	8
NT												6.03	8	3.54	2.4	672.3	189.9	39.2	0.7	1.5	8
06																		40.0			
AR																		100.8			
EL.												3.48	171	3.63	8.5	391.8	187.9	15.8	1.8	1.0	8
																					_
	83	VII	8 5	16	48	6.6	24.	135	67.05	183	4.8							42.5			
	NO.											8.61	331	3,55	3.1	974.0	274.4	57.8	1.8	3.2	6
RE	90														_						
	40											29.38	346	3.63				15.0 10.0	4.5	.3.6	

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LPB 83 VII 86 85 54 55.8 24.178 67.89 189 4.4 7.65 353 3.64 8.5 849.1 233.3 22.5 8.8 3.29 C
                                           8.71 331 3.52 2.8 986.8 279.8 27.2 0.9 2.16 C
ARE
B06
                  NO La
                                           29.48 346 3272.1
CAR
                                           34.58 8 3.64 1.3 3837.9 1955.3 18.6 8.8 4.21 C
LPB 83 VII 87 84 58 37.8 28.695 68.96 112 4.9 4.21 11 3.53 2.5 488.9 136.2 568.8 8.7 4.92 B
ARE
                                           4.84 338 3.37 2.4 549.3 162.8 637.5 0.9 4.98 C
806
                  NO La
                                           25.60 348
                                                             2845.6
CAR
                                           31.10 4 3.63 8.5 3457.3 953.3 19.8 1.2 2.92 C
LPB 83 VII 88 82 03 16.0 28.785 69.58 82 5.2 3.76 21 3.68 8.8 425.7 115.7 1326.8 8.9 4.84 C
                                            3.72 193 3.63 1.2 458.8 116.3 91.5 8.8 2.64 C
                                           4.07 332 3.56 7.6 459.6 129.0 1025.0 1.1 4.49 C
HeF
CAR
                                           30.49 5 3.63 0.7 3528.7 934.0 71.5 1.5 3.32 C
808
                                           24.95 349 3.41 1.8 2773.4 B13.6 98.8 1.3 3.56 C
LPB 83 VII 15 23 41 9.5 23.105 68.20 172 --- 6.56 1 3.59 2.1 748.9 208.5 62.0 1.2
MNA
                                         13.86 322 3.68 5.6 1542.9 428.5 49.5 1.5
LPB 83 VII 19 04 33 24.5 22.065 68.49 126 4.7 5.51 4 3.62 4.8 625.0 172.5 100.0 1.1 ± 56 C
                                           6.25 333 3.61 15.3 705.8 195,5 185.3 0.9 4.35 C
CAR
                                           32.4B 3 3.6B 2.2 36B2.2 18B5.8 21.7 B.7 3.9B C
LPA
                                           15.88 146 3.62 5.6 1769.8 485.8 126.8 1.4 4.26 C
                                           12.80 320 3.61 3.5 1427.8 395.5 33.7 1.4 2.96 C
NNA
LPB 83 VII 19 20 21 28.8 24.235 67.07 192 4.3 7.72 352 3.57 0.4 878.9 246.5 40.0 1.0 3.78 C
ARE
                                           8.78 331 3.49 5.2 994.3 284.7 94.6 1.8 4.10 C
CAR
                                           34.50 0 3.62 0.6 3838.1 1058.0 32.5 1.1 4.63 B
LPA
                                           13.39 145 3.62 1.1 1490.2 411.2 48.8 4.8 4.50 B
NNA
                                           15.30 321 3.6i 1.9 1710.8 473.2 77.4 1.8 4.09 C
LPB 83 VII 19 22 10 39.3 20.655 69.50 158 --- 4.30 18 3.60 1.4 503.2 139.7 53.0 1.1
                                           4.57 335 3.39 5.2 531.8 156.7 142.0 1.0
ARE
CAR
                                           31.10 5 3.60 6.6 3458.8 960.0 129.0 1.8
LPA
                                          17.50 147 3.56 1.0 1950.2 545.7 42.0 0.8
                                          11.10 320 3.56 6.4 1242.4 345.7 198.7 1.7
LPB 83 VII 28 85 48 52.5 22.885 68.85 128 4.7 6.28 7 3.63 6.5 789.4 195.5 137.5 1.1 3.92 C
ARE
                                           6.79 338 3.63 9.1 765.2 218.5 60.3 0.9 3.45 B
CAR
                                           33.20 3 3.57 1.0 3691.1 1032.5 84.5 1.6 4.38 C
LPA
                                          15.40 144 3.56 0.9 1715.9 480.5 36.0 0.8 3.64 C
NNA
                                          13.20 323 3.55 2.8 1472.2 412.5 52.0 1.6 3.25 C
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25.88 5 3.56 1.1 3978.3 1116.8 88.8 1.5 14.28 135 3.58 0.9 1579.3 441.0 33.6 8.5 14.78 135 3.58 0.9 1579.3 441.0 33.6 8.5 14.78 333 3.58 1.7 1633.4 456.8 33.7 1.4 33.6 8.5 14.78 333 3.58 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 1.2 31.3 16.8 1.3 16.8 1.3 1.2 31.3 16.8 1.3 16.8 1.3 1.2 31.3 16.8 1.3 16.8 1.3 1.2 31.3 16.8 1.3 16.8 1.3 1.2 31.3 16.8 1.3 16.8 1.3 1.2 31.3 16.8 1.3 1.2 16.2 16.8 1.3 16.8 1.3 16.8 1.3 16.8 1.3 16.8 1.3 16.8 1.3 16.8 1.3 16.8 1.3 16.8 1.3 16.8 16.8 16.8 16.8 16.8 16.8 16.8 16.8																					
8. 95 352 3.48 4.6 996.8 295.8 53.2 1.1 8. 95 352 3.48 4.6 996.8 295.8 53.2 1.1 8. 25.88 5 3.56 1.1 3978.3 1116.8 88.0 1.5 14.70 333 3.58 1.7 1633.4 456.0 33.7 1.4 8. 88 3 VII 21 87 11 32.3 22.345 68.54 119 5.5 5.79 4 3.68 4.7 654.2 181.7 3116.8 1.3 4.99 8. 83 VII 21 87 11 32.3 22.345 68.54 119 5.5 5.79 4 3.68 4.7 654.2 181.7 3116.8 1.3 4.99 8. 4.7 333 3.58 1.7 633.4 456.0 33.7 1.4 8. 88 3 VII 21 87 11 32.3 22.345 68.54 119 5.5 5.79 4 3.68 4.7 654.2 181.7 3116.8 1.3 4.99 8. 4.7 333 3.58 1.7 633.4 456.0 33.7 1.4 8. 88 3 VII 21 87 11 32.3 22.345 68.54 119 5.5 5.79 4 3.68 4.7 654.2 181.7 3116.8 1.3 4.99 8. 8 1 1 28 83 29 41.8 4.585 38.38 80 5.2 31.63 245 3.57 6.4 3514.4 983.2 1625.8 1.6 6.88 8. 8 1 1 29 83 29 41.8 4.585 38.38 80 5.2 31.63 245 3.57 6.4 3514.4 983.2 1625.8 1.6 6.88 8. 8 2 1 2 2 8 3 2 9 41.8 4.585 38.38 80 5.2 31.63 245 3.57 6.4 3514.4 983.2 1625.8 1.6 6.88 8. 8 2 1 2 2 2 3 2 3 2 3 3 3 3 3 3 3 3 3 3 3	PB	83	VII	28	22	11	54.8	25.375	78.28	69	~~~	9.81	13	3.68	1.6	1003.5	278.6	28.∎	8.7		c
25.88 5 3.56 1.1 3978.3 1116.8 88.8 1.5 14.28 135 3.58 0.9 1579.3 441.0 33.6 8.5 14.78 135 3.58 0.9 1579.3 441.0 33.6 8.5 14.78 333 3.58 1.7 1633.4 456.8 33.7 1.4 33.6 8.5 14.78 333 3.58 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 33.7 1.4 38 88 81 1.7 1633.4 456.8 1.2 31.3 16.8 1.3 16.8 1.3 1.2 31.3 16.8 1.3 16.8 1.3 1.2 31.3 16.8 1.3 16.8 1.3 1.2 31.3 16.8 1.3 16.8 1.3 1.2 31.3 16.8 1.3 16.8 1.3 1.2 31.3 16.8 1.3 1.2 16.2 16.8 1.3 16.8 1.3 16.8 1.3 16.8 1.3 16.8 1.3 16.8 1.3 16.8 1.3 16.8 1.3 16.8 1.3 16.8 16.8 16.8 16.8 16.8 16.8 16.8 16.8	RE		•••			••		2010.0													C
14.20 135 3.58 0.9 1579.3 441.6 33.6 0.5 14.70 333 3.58 1.7 1633.4 456.0 33.7 1.4 18 83 VII 21 07 11 32.3 22.345 68.54 119 5.5 5.79 4 3.68 4.7 654.2 181.7 3116.8 1.3 4.99 18 6.47 334 3.58 1.5 728.7 207.7 318.0 1.2 3.13 36.28 3 3.64 3.2 4032.9 1107.7 205.2 2.0 3.59 15.60 146 3.55 2.3 1737.4 407.7 640.0 1.8 4.51 12.98 321 3.58 3.8 1447.1 404.5 123.7 1.5 2.68 18 88 XI 20 03 29 41.8 4.505 38.30 00 5.2 31.63 245 3.57 6.4 3514.4 983.2 1625.0 1.6 6.80 18 88 XI 20 03 29 41.8 4.505 38.30 00 5.2 31.63 245 3.57 6.4 3514.4 983.2 1625.0 1.6 6.80 18 88 XI 20 03 29 41.8 4.505 38.30 00 5.2 31.63 245 3.57 6.4 3514.4 983.2 1625.0 1.6 6.80 18 88 XI 20 03 29 41.8 4.505 38.30 00 5.2 31.63 245 3.57 6.4 3514.4 983.2 1625.0 1.6 6.80 18 88 XI 20 03 29 41.8 4.505 38.30 00 5.2 31.63 245 3.57 6.4 3514.4 983.2 1625.0 1.6 6.80 18 88 XI 20 03 29 41.8 4.505 38.30 00 5.2 31.63 245 3.57 6.4 3514.4 983.2 1625.0 1.6 6.80 18 88 XI 20 03 29 41.8 4.505 38.30 00 5.2 31.63 245 3.57 6.4 3514.4 983.2 1625.0 1.6 6.80 18 88 XI 20 03 29 41.8 4.505 38.30 00 5.2 31.63 245 3.57 6.4 3514.4 983.2 1625.0 1.6 6.80 18 88 XI 20 03 29 41.8 4.505 38.30 00 5.2 31.63 2.2 3724.4 1040.3 115.0 1.2 4.42 18 88 XI 30 05 19 48.3 5.505 35.78 5 4.9 33.52 248 3.58 2.2 3724.4 1040.3 115.0 1.2 4.55 18 80 XI 30 05 19 48.3 5.505 35.78 5 4.9 13.63 248 3.75 2.3 1124.7 296.2 35.0 1.2 4.42 18 10 10 16 16 3.75 2.3 1124.7 296.2 35.0 1.1 2.80 18 10 10 15 06 11 16.8 10.125 76.47 117 5.5 10.34 129 3.52 4.6 1154.8 328.2 520.0 1.0 4.04 18 10 10 15 06 11 16.8 10.125 76.47 117 5.5 10.34 129 3.52 4.6 1154.8 328.2 520.0 1.0 3.17 18 10 10 10 10 10 10 10 10 10 10 10 10 10												25.00	5	2 54	1.1	2070 2	1115 0	50.2 50.0	1.5		C
14.78 333 3.58 1.7 1633.4 456.8 33.7 1.4 18 83 VII 21 07 11 32.3 22.345 68.54 119 5.5 5.79 4 3.68 4.7 654.2 181.7 3116.8 1.3 4.99 18 83 VII 21 07 11 32.3 22.345 68.54 119 5.5 5.79 4 3.68 4.7 654.2 181.7 3116.8 1.3 4.99 18 83 VII 21 07 11 32.3 22.345 68.54 119 5.5 5.79 4 3.68 4.7 654.2 181.7 3116.8 1.3 4.99 18 83 VII 20 03 29 41.8 4.505 38.38 00 5.2 31.63 245 3.57 6.4 3514.4 983.2 1625.0 1.6 6.80 12.98 321 3.58 3.8 1447.1 484.5 123.7 1.5 2.68 8 88												14 70	125	3.00	1.1	1570 2	1110.0	22.5	1.0		C
BR 83 VII 21 07 11 32.3 22.345 68.54 119 5.5 5.79 4 3.68 4.7 655.2 181.7 3116.8 1.3 4.99 6.47 334 3.58 1.5 728.7 207.7 310.0 1.2 3.13 36.28 3 3.64 3.2 4932.9 1197.7 205.2 2.8 3.59 15.60 146 3.56 2.3 1737.4 487.7 648.0 1.8 4.51 12.98 321 3.58 3.8 1447.1 404.5 123.7 1.5 2.68 88 XI 20 03 29 41.8 4.505 38.38 00 5.2 31.63 245 3.57 6.4 3514.4 983.2 1625.0 1.6 6.00 34.71 247 3.69 5.1 3856.6 1844.3 495.0 2.5 4.67 32.16 298 3.64 2.0 3573.3 980.7 283.0 1.5 4.27 288 86 XI 30 05 19 48.3 5.505 35.78 5 4.9 33.52 248 3.58 2.2 3724.4 1840.3 115.0 1.2 4.55 34.86 297 3.44 10.3 3873.3 1121.0 103.0 1.8 4.13 20 05 19 48.3 5.505 75.00 75 4.8 11.60 149 3.47 5.1 1291.1 372.1 205.0 1.2 4.42 20 05 05 11 16.8 10.125 76.47 117 5.5 10.34 129 3.52 4.6 642.2 176.2 161.0 0.8 4.09 120 120 120 120 120 120 120 120 120 120												14.70	150	3.40	17	1012.0	451.0	70.0	1 4		
## 88 VI 21 W7 11 32.3 22.345 68.54 119 5.5 5.79 4 3.68 4.7 654.2 181.7 3116.8 1.3 4.99	RM											14.76	333	3.38	1.7	1033.4	420.10	33.1	1.4		·
8E																					
36.28 3 3.64 3.2 4832.9 1107.7 205.2 2.0 3.59 PA 15.60 146 3.56 2.3 1737.4 487.7 648.0 1.0 4.51 12.98 321 3.58 3.8 1447.1 404.5 123.7 1.5 2.60 BRASIL PB 88 XI 20 03 29 41.8 4.505 38.38 00 5.2 31.63 245 3.57 6.4 3514.4 983.2 1625.0 1.6 6.00 BRASIL PB 86 XI 30 05 19 48.3 5.505 35.70 5 4.9 33.52 248 3.50 5.1 3856.6 1044.3 495.0 2.5 4.67 32.16 298 3.64 2.0 3573.3 980.7 203.0 1.5 4.27 PB 86 XI 30 05 19 48.3 5.505 35.70 5 4.9 33.52 248 3.50 2.2 3724.4 1040.3 115.0 1.2 4.55 34.86 297 3.44 10.3 3073.3 1121.0 103.0 1.8 4.13 PERU-BRASIL PB 78 V 28 06 07 3.0 6.705 75.00 75 4.8 11.60 148 3.47 5.1 1291.1 372.1 205.0 1.2 4.42 10.10 164 3.76 2.3 1124.7 296.2 35.0 1.1 2.86 5.74 204 3.64 2.0 642.2 176.2 161.0 0.8 4.09 PB 82 VIII 15 06 11 16.8 10.125 76.47 117 5.5 10.34 129 3.52 4.6 1154.8 320.2 520.0 1.0 4.04 NO Lg 1.69 191 240.4 14.69 158 3.60 3.7 261.3 710.2 247.0 2.5 3.20 EL 23.52 168 3.60 3.7 261.3 710.2 247.0 2.5 3.20 25.50 36 3.63 2.2 2035.7 700.4 608.0 1.8 4.41 PB 83 III 20 01 56 38.6 10.485 74.88 18 5.4 8.90 133 3.55 12.8 909.0 278.4 372.3 0.9 3.93 2.44 232 3.60 1.2 271.7 75.4 170.0 1.0 2.79	RE		•••		•					•••											
15.60 146 3.56 2.3 1737.4 487.7 648.0 1.0 4.51 12.98 321 3.58 3.8 1447.1 404.5 123.7 1.5 2.60 BRASIL																					
BRASIL BRASIL																					
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PB 78	ar 											34.86	297	3.44	18.3	3873.3	1121.8	103.0	1.8	4.13	3
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														700.0	4/3.0		V: UT
														417.8			
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									15.11					484.0			
														719.8			
														884.8			
									13.70	163	3.48	2.8	1522.2	447.8	33.7	1.4	2.11
									6.65	152	3.66	18.9	740.1	202.0	595.2	1.2	4.26
									15.13	3	3.63	8.7	1681.1	462.0	288.5	1.5	4.26
									22.37	21	3.61	0.7	2485.6	688.8	49.6	1.2	2.94
									21.70	150	3.59	1.6	3188.9	887.0	136.8	1.3	3.96
									2.44	235	3.61	3.5	271.3	69.0	118.2	1.3	2.10
									22.76	171	3.58	8.1	2528.9	707.3	48.7	1.6	2.69
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								5.1	10.02	143	3.58	6.1	1123.6	313.8	362.5	1.1	4.35
									13.10	1	3.50	2.1	1463.5	417.5	155.8	1.2	3.72
									24.78	173	3.62	6.8	2741.6	758.8	52.8	1.6	2.99
AII	13	40	10	34.1	17.635	/1.3/	/6										
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						··· -			7.18	164	3.62	8.4	734.2	219.0	7.8	9.6	
									27.78	12	3,56	3.1	3279.1	864.0	67.5	1.4	
									6.48	318	3,60	1.5	717.6	133.0	12.5	1.1	
	VII VIII	V 21 VI 21 VII 15	V- 21 28 VI 21 09 VII 15 28	V- 21 28 85 VI 21 89 23 VII 15 28 16	V- 21 28 85 13.8 VI 21 89 23 56.2 VII 15 28 16 54.1	V- 21 28 85 13.8 18.59S VI 21 89 23 56.2 8.56S VII 15 28 16 54.1 17.63S	VI 21 09 23 56.2 8.565 74.38 VI 21 09 23 56.1 17.635 71.57 XII 03 18 39 51.8 17.615 69.51	V- 21 28 85 13.8 18.59\$ 74.79 18 VI 21 89 23 56.2 8.56\$ 74.38 152 VII 15 28 16 54.1 17.63\$ 71.57 78 XII 83 18 39 51.8 17.61\$ 69.51 178	V- 21 28 85 13.8 18.59\$ 74.79 18 5.2 VI 21 89 23 56.2 8.56\$ 74.38 152 5.1 VII 15 28 16 54.1 17.63\$ 71.57 78 4.8 XII 83 18 39 51.8 17.61\$ 69.51 178	V-21 28 85 13.8 18.598 74.79 18 5.2 8.79 13.70 6.65 15.13 22.37 21.70 2.44 22.76 VI 21 89 23 56.2 8.568 74.38 152 5.1 18.82 8.34 13.18 20.34 24.78 VII 15 28 16 54.1 17.638 71.57 78 4.8 3.58 7.58 35.92 XII 83 18 39 51.8 17.618 69.51 178 1.72 6.18 28.10 9.83 XII 85 87 88 31.8 16.888 72.58 92 4.23 7.18	V 21 28 85 13.8 18.59S 74.79 18 5.2 8.79 133 13.70 163 6.65 152 15.13 3 22.37 21 21.70 150 2.44 235 22.76 171 VI 21 89 23 56.2 8.56S 74.38 152 5.1 18.82 143 8.34 161 13.18 1 20.34 27 24.78 173 VII 15 28 16 54.1 17.63S 71.57 78 4.8 3.58 72 7.58 317 35.92 9 XII 83 18 39 51.8 17.61S 69.51 178 1.72 52 6.18 188 28.10 5 9.83 387	V 21 28 95 13.8 18.59\$ 74.79 18 5.2 8.79 133 3.62 13.70 163 3.48 6.65 152 3.66 15.13 3 3.63 22.37 21 3.61 21.70 150 3.59 2.44 235 3.61 22.76 171 3.58 VI 21 89 23 56.2 8.56\$ 74.38 152 5.1 18.82 143 3.58 8.34 161 3.59 13.18 1 3.50 20.34 27 3.51 24.70 173 3.62 VII 15 28 16 54.1 17.63\$ 71.57 78 4.8 3.58 72 3.59 7.58 317 3.44 35.92 9 3.67 XII 83 18 39 51.8 17.61\$ 69.51 178 1.72 52 3.61 6.18 188 3.61 28.10 5 3.56 9.83 387 3.53	V 21 28 85 13.8 18.595 74.79 18 5.2 8.79 133 3.62 6.4 13.70 163 3.48 2.8 6.65 152 3.66 18.9 15.13 3 3.63 8.7 22.37 21 3.61 0.7 21.70 150 3.59 1.6 2.44 235 3.61 3.5 22.76 171 3.58 8.1 VI 21 89 23 56.2 8.565 74.38 152 5.1 18.82 143 3.58 6.1 8.34 161 3.58 2.2 13.10 1 3.50 2.1 20.34 27 3.51 1.3 24.70 173 3.62 6.8 VII 15 28 16 54.1 17.635 71.57 78 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748.1 202.0 15.13 3.63 8.7 1681.1 462.0 22.37 21 3.61 0.7 2485.6 688.0 21.70 150 3.59 1.6 3188.9 887.0 2.44 235 3.61 3.5 271.3 69.0 22.76 171 3.58 8.1 2528.9 707.2 22.76 171 3.58 8.1 2528.9 707.2 22.76 171 3.58 8.1 2528.9 707.2 22.76 171 3.58 8.1 2528.9 707.2 22.76 171 3.58 8.1 2528.9 707.2 22.76 171 3.58 8.1 2528.9 707.2 22.76 171 3.58 8.1 2528.9 707.2 22.76 171 3.58 8.1 2528.9 707.2 22.76 171 3.58 8.1 2528.9 707.2 22.76 171 3.58 2.2 93.6 6.4 13.10 1 3.50 2.1 1463.5 417.6 20.34 27 3.51 1.3 2265.1 644.4 24.70 173 3.62 6.0 2741.6 758.8 24.70 173 3.62 6.0 2741.6 758.8 25.92 9 3.67 1.0 3991.7 1085.9 25.92 9 3.67 1.0 3991.7 1085.9 25.91 10.92 10.93 10.9	V 21 28 85 13.8 18.59S 74.79 18 5.2 8.79 133 3.62 6.4 976.6 269.8 268.8 88.8 V 21 28 85 13.8 18.59S 74.79 18 5.2 8.79 133 3.62 6.4 976.6 269.8 268.8 V 21 28 85 13.8 18.59S 74.79 18 5.2 8.79 133 3.62 6.4 976.6 269.8 268.8 13.78 163 3.48 2.8 1522.2 447.8 33.7 6.65 152 3.65 18.9 748.1 202.0 595.2 15.13 3 3.63 8.7 1681.1 462.0 288.5 22.37 21 3.61 0.7 2485.6 688.0 49.6 21.78 158 3.59 1.6 3188.9 887.8 136.8 2.44 235 3.61 3.5 271.3 69.8 118.2 22.76 171 3.58 8.1 2528.9 787.3 48.7 VI 21 89 23 56.2 8.565 74.38 152 5.1 18.82 143 3.58 6.1 1123.6 313.8 362.5 8.34 161 3.58 2.2 939.8 268.4 115.8 13.10 1 3.58 2.1 1463.5 417.6 155.8 28.34 27 3.51 1.3 2265.1 644.4 92.0 24.78 173 3.62 6.8 2741.6 758.8 52.8 VII 15 28 16 54.1 17.635 71.57 78 4.8 3.58 72 3.58 3.7 395.1 112.9 688.8 VII 83 18 39 51.8 17.615 69.51 178 1.72 52 3.61 1.5 261.2 72.3 888.8 XII 83 18 39 51.8 17.615 69.51 178 1.72 52 3.61 1.5 261.2 72.3 888.8 XII 83 18 39 51.8 17.615 69.51 178 1.72 52 3.61 1.5 261.2 72.3 888.8 XII 83 18 39 51.8 17.615 69.51 178 4.23 86 3.68 2.8 478.9 133.8 34.0 47.2 XII 85 87 88 31.8 16.88S 72.58 92 4.23 86 3.68 2.8 478.9 133.8 84.8 7.18 164 3.62 8.4 794.2 219.0 7.8	2.46 335 3.69 2.2 273.5 74.8 318.8 1.2 22.78 171 3.48 2.4 2531.1 728.6 88.8 1.5 V 21 28 85 13.8 18.595 74.79 18 5.2 8.79 133 3.62 6.4 976.6 269.8 268.8 1.5 13.78 163 3.48 2.8 1522.2 447.8 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ECUADOR

I PR 83	VII 21 86 46	4.9	1.335 88.99	54 5.8 19.74 141 3.55	1.3 2194.8	617.6	165.0 1.5 4.06 C
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							186.0 1.2 3.96 B
NNA				11.30 133 3:00	111 120011		

Lg apparent velocity and normalized amplitude appear independent of the distance in spite of data dispersion, as it appears in figures 6 and 7 .

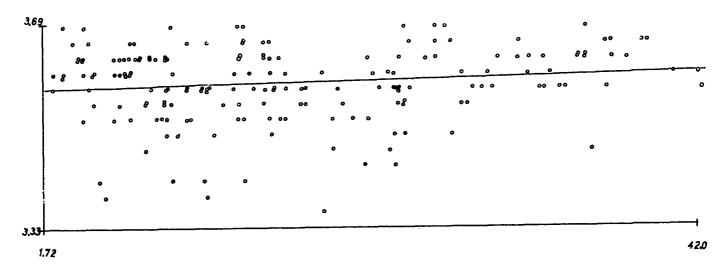


Fig. 6 .- Lg apparent velocity vs. distance.

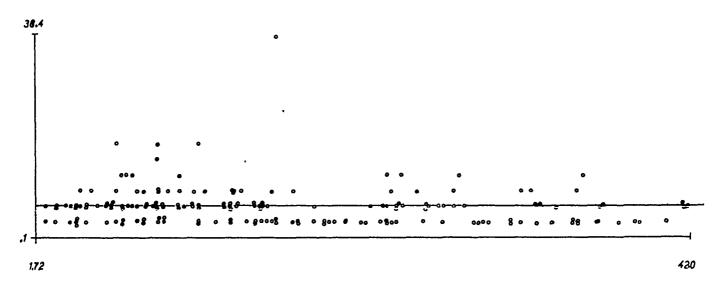


Fig. 7 .- Lg/P vs. distance.

Comparison of Lg/P and e is presented in fig. 8, again with a high data dispersion.

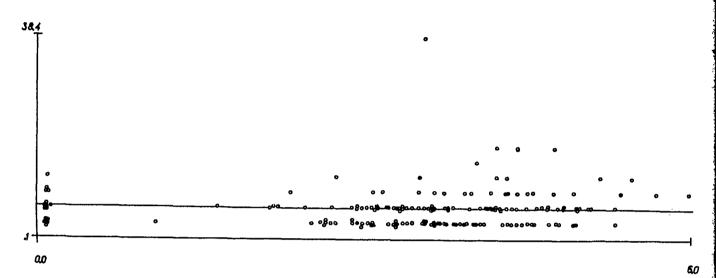


Fig. 8 .- Lp/P vs. energy.

Table III shows the frequency of occurrence of each apparent velocity interval; practically data extends between 3.48 and 3.68 km/s, what may seem a too broad range, but it happens because in most cases Lg has an emergent character.

Table III .- Lg apparent velocity.

CLASS	LIMITS ====	FREQUENCY	PERCENT	(4)
3.30	- 3.32	Ω	.00	***
3.32	- 3.34	1	.56)•
3.34	- 3.36	i	.56	ή•
3.36	- 3.38	i	.56	í.
3.38	- 3.40	ż	1.13	1
3.40	- 3.42	3	1.69	1
3.42	- 3.44	ž	1.13)••
3.44		ă	2.26	1
				,
3.46	- 3.48	2 5	1.13)
3.48	- 3.50	5	2.82)****
3.50	- 3.52	12	6.78)
3.52	- 3.54	9	5.08)
3.54	- 3.56	13	7.34	
3.56	3.58	2.3	12.99)
3.58	- 3,60	14	7.91)
3,60	- 3.62	22	12.43	jerreenaassereessaasse
3.62	- 3.64	25	14.12	
3.64	- 3.66	15	8.47	
3,66	- 3,68	14	7.91	1
3,68	- 3.70	9	5.08	1
5,	тот		100.00	,

Table IV sets off that commonly Lg amplitude equals P amplitude (in South America in many cases Rg phase is much larger than Lg; it should be carefully analysed in the future). An exception of abnormally high Lg/P = 38 acquires a special relief.

Table IV .- Normalized amplitude Lg/P

====CLASS	LIMI	TS====	FREQUENCY	PERCENT	(#)
.00	-	1.00	25	14.12	` ;	
1.00	-	2.00	54	30.51	•	,
2.00	-	3.00	32	18.08	•	
3.00	-	4.00	16	9.04	•) * # * * # # # # # # # # # # # # # # #
4.00	-	5.00	14	7.91	•	
5.00	-	6.00	11	6.21) = = = =
6.00	-	7.00	10	5.65) = = = = = = = = = = = = = = = = = = =
7.00	-	8.00	2	1.13	•) =
8.00	-	9.00	4	2.26	•) * *
9.00	-	10.00	2	1.13	•) =
10.00	-	11,00	2	1,13) =
11.00	-	12.00	0	.00)
12.00	-	13.00	1	.56)
13.00	-	14.00	0	.00)
14.00	-	15.00	0	.00)
15.00	-	16.00	1	.56	•)
16.00	-	17.00	1	.56	•)
17.00	-	18.00	1	.56	•)
38.00	-	39.00	1	.56)
		TO	TAL 177	100.00		
						- -

Looking for a more detailed analysis, it will be convenient to consider Lg characteristics separately both by seismogenic regions and by recording stations; actually most of wave paths are partly cordilleran and partly shield.

Table V Number of each Lg character in South America stations STA CHARACTER TOTAL C В LPB 12 10 19 41 ANT 1 4 5 10 ARE Ø 14 13 27 BOG Ø 3 7 10 CAR g 6 5 11 NNA Ø 7 13 20 PEL 1 Ø 8 9 QUI Ø 1 Ø 1 SJG Ø ø 4 4 TRN 4

Table VI shows together apparent velocity, normalized amplitude and normalized energy according to origin regions. It merits some comments:

It is evident that Lg velocity is the same either for all the origin regions or for all the stations considered, since the largest standard deviation calculated was $\theta.\theta = 0.05$ km/s in ARE less than for LPB and $\theta.\theta = 0.05$ km/s in SJG more than for LPB.

Table VI

REGION	Lį	y VELO	CITY		Lg/P			ENERG	Y	NO.
	min	ma x	mean	min	ma x	mean	min	ma x	mean	MEASURES
Colombia	3.43	3.66	3.56	Ø.5	8.3	2.4	2.4	5.4	3.7	19
Venezuela	3.48	3.68	3.60	1.9	9.5	4.2	3.3	5 3	4.6	9
Argentina	3.33	3.68	3.6Ø	Ø.2	8.1	2.6	2.4	5.2	3.6	32
Chile	3.37	3.69	3.58	Ø.1	33.4	3.9	Ø	5.6	3.Ø	65
Brazil	3.44	3.69	3.58	2.0	10.3	5.2	4.1	6.Ø	4.7	5
Peru	3.40	3.76	3.58	Ø.2	12.Ø	3.4	Ø	.4.7	3.2	42
Ecuador	3.55	3.59	3.57	Ø.7	1.5	1.2	3.Ø	4.1	3.7	5

Amplitude Lg/P is larger in LPB than in the other stations in 72 cases, is minor in 28 cases (for $2\emptyset$ earthquakes among 41 LPB has the largest normalized amplitude).

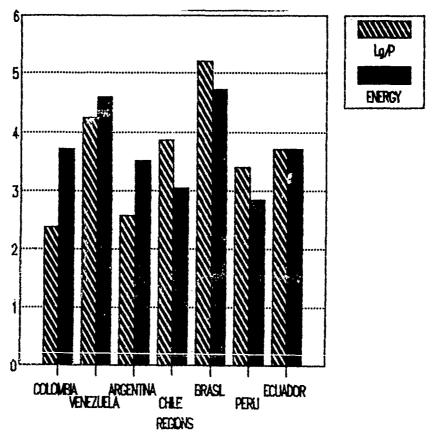


Fig. 9 .- Energy and Lg/P .

Fig. 9 shows the normalized Lg/P and e, but we have to remark again that data for Brazil (reasonable) and Ecuador (unreasonable) are not representative, because they are supported by a small number of cases.

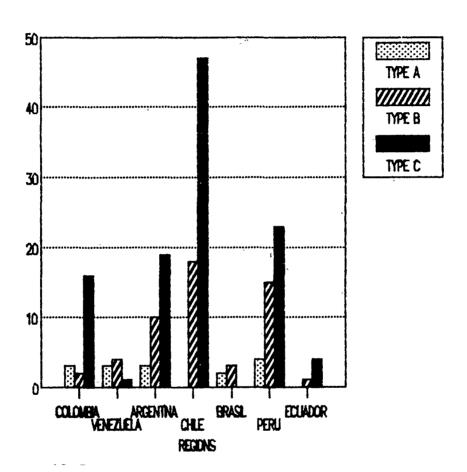


Fig. 10 .- Character of Lg according to origin regions.

Fig. 16 shows the type of Lg recording. We see that for most of the region type C is prevalent, but not so for Venezuela and Brazil.

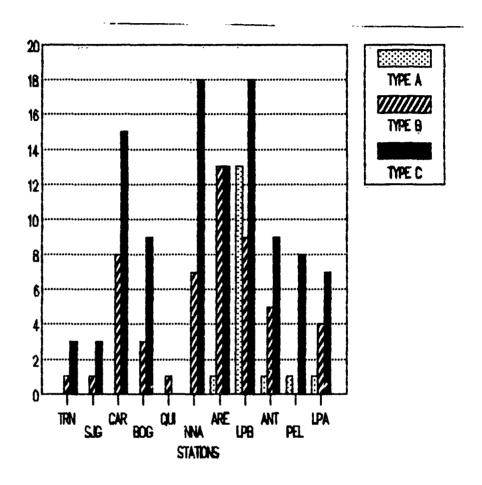


Fig. 11 .- Character of Lg in recording stations.

The Fig. 11 shows the frequency of each type of recording in the stations revised.

Fig. 12 shows schematically South America structure; it has been adapted from Alcocer (1989).

Fig. 13 and 14 show Lg paths epicenter-station, with the indication of Lg recording character. Comparison with fig. 12 is self explanatory.

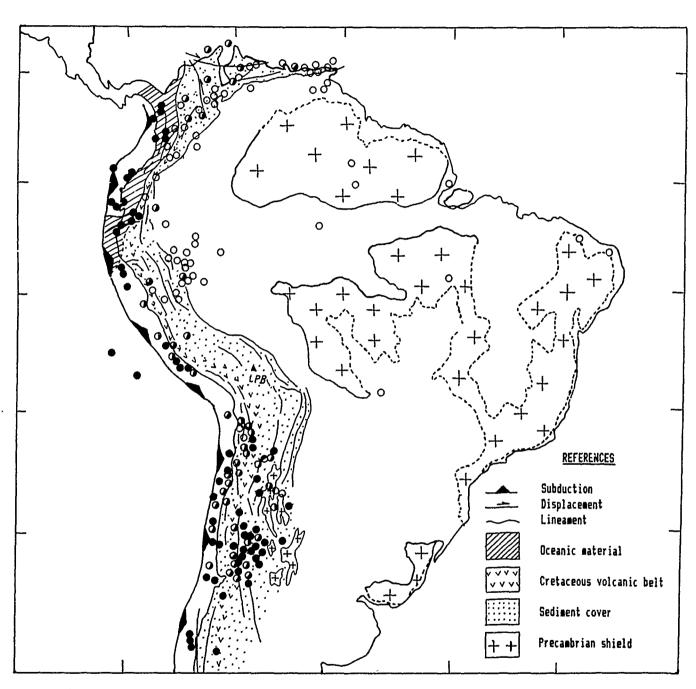


Fig. 12 .- South American tectonic structure (adapted from Alcocer, 1989).

O Type A: efficiency transmission of Lg
 O Type B: mean efficiency transmission of Lg
 ● Type C: inefficiency transmission of Lg

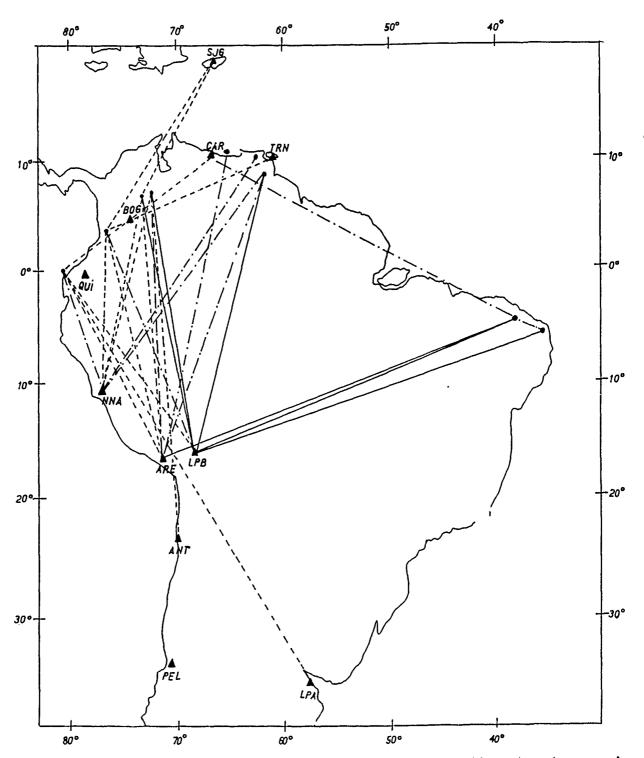


Fig. 13 .- Paths from northern part of South America and recording type.

Efficiency path

Median efficiency path
Inefficiency path
Epicenter
Station

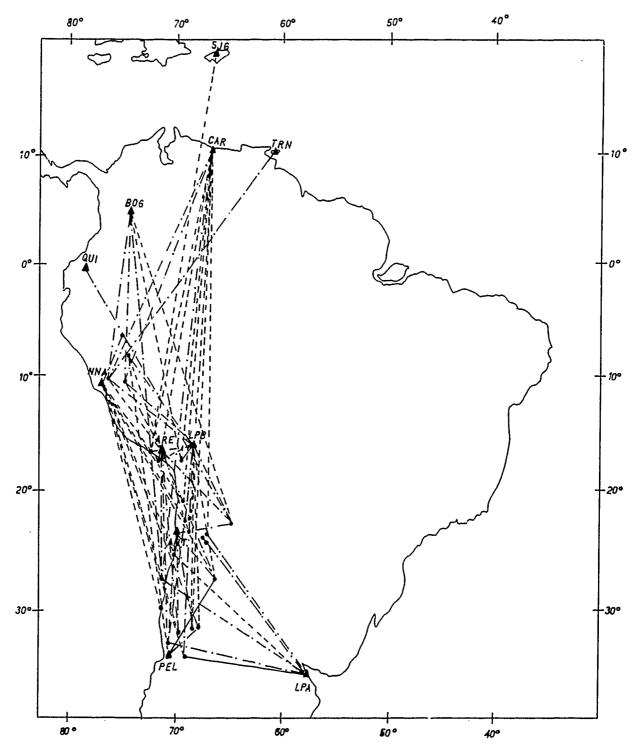


Fig. 14 .- Paths from southern part of South America and recording type.

Efficiency path

Median efficiency paths

Inefficiency paths

Epicenter

Station

LPB, a privileged station?

A question arises from several points in the present report: why La Paz is in a better condition than other stations both concerning the amplitude and the clearer type of Lg.

Looking for a convincing answer, we acknowledge that LPB is running on the cordilleran structure not far from its border, that is to say, cordilleran path is short, then it should attenuate waves by absorbing their energy, not destroying such energy, but changing it trough a local enlargement of waves. They may appear an antinomy, but a similar phenomenon is well known in local earthquakes when the higher is the attenuation the stronger are destructive effects.

Conclusions

Lg.

Lg phase is made up of transverse waves, SH type, guided within a layer in the continental crust.

Mean apparent velocity is 3.57 km/s; extreme values are 3.35 and 3.69 km/s. It does not change either for seismogenic regions or for recording stations.

Predominant period in LPB is 1.1 to 1.3; in several cases it is shorter to 0.7 s or longer to 2.5 s.

Normalized amplitude Lg/P in general approaches unity, (though it exceptionally reached 38). It depends on the path nature.

In general it is coherent with Bath's normalized energy. Brasilian and Guayana Shield are efficient transmitters of

Western Colombia and Ecuador earthquakes give poor Lg records, apparently because of the difficulty of generation rather than of transmission.

Argentinian and Chilean earthquakes have a cordilleran path to La Paz; such path is inefficient for shorter periods, not so much for longer periods until 2.5 s.

Earthquakes from Peru and Peru-Brazil Border give uneven Lg in LPB, probably because of crustal structure complexities, but prevailing a transmission of medium efficiency.

Lg may originate for earthquakes deep almost 200 km in subduction zones.

Comparison of Lg recording in South America stations shows clearer and larger Lg waves in LPB for most of earthquakes. It is interpreted as an effect of local attenuation within a short cordilleran path.

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